



A basic control system

Control system specifications

2 Disturbance models

- Stochastic processes
- Filtering of white noise
- Spectral factorization



- Controller: feedback C, feedforward F
- Process: transfer function P
- Process/load disturbance *d*: drives system from desired state
- Controlled process variable *z*: should follow reference *r*
- Measurement noise *n*: corrupts information about *z*

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A more general setting

Process disturbances need not enter at the process input, and measurement noise and setpoint values may also enter in different ways. More general setting:



We will return to this setting later in the course

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Design specifications

Find a controller that

- A: reduces the effect of load disturbances
- B: does not inject too much measurement noise into the system
- C: makes the closed loop insensitive to process variations
- **D:** makes the output follow the setpoint

Common to have a controller with **two degrees of freedom** (2 DOF), i.e. separate signal transmission from y to u and from r to u. This gives a nice separation of the design problem:

- Design feedback to deal with A, B, and C
- Design feedforward to deal with D



Some systems only allow error feedback



Relations between signals



Atomic Force Microscope



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Only the control error can be measured

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Design of disturbance attenuation and setpoint response cannot be separated



The "Gang of Four" / "Gang of Six"



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Some observations

 $Z = \frac{P}{1 + PC}D - \frac{PC}{1 + PC}N + \frac{PCF}{1 + PC}R$

 $Y = \frac{P}{1 + PC}D + \frac{1}{1 + PC}N + \frac{PCF}{1 + PC}R$

 $U = -\frac{PC}{1+PC}D - \frac{C}{1+PC}N + \frac{CF}{1+PC}R$

Four transfer functions are needed to characterize the response to load disturbances and measurement noise:

$$\frac{PC}{1+PC} \qquad \frac{P}{1+PC} \\ \frac{C}{1+PC} \qquad \frac{1}{1+PC}$$

Two more are required to describe the response to setpoint changes (for 2-DOF controllers):

$$\frac{PCF}{1+PC} \qquad \frac{CF}{1+PC}$$

- To fully understand a control system it is necessary to look at **all** four or six transfer functions
- It may be strongly misleading to show properties of only one or a few transfer functions, for example only the response of the output to command signals. (This is a common error.)
- The properties of the different transfer functions can be illustrated by their frequency or time responses.



Example: Frequency Responses



Example: Time Responses

PI control ($K_p = 0.775$, $T_i = 2.05$) of $P(s) = (s + 1)^{-4}$ with $G_{yr}(s) = (0.5s + 1)^{-4}$. Gain curves:



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Time responses—an alternative

Responses to setpoint step, load disturbance step and random measurement noise:



Error feedback (dashed), 2-DOF controller (full)

One plot gives a good overview!

Pl control ($K_p = 0.775$, $T_i = 2.05$) of $P(s) = (s + 1)^{-4}$ with $G_{vr}(s) = (0.5s + 1)^{-4}$. Step responses:



Remember to always look at **all** responses when you are dealing with control systems. The step response below looks fine, but...





A warning - Gang of Four



A warning - The system

Step responses:



Unstable output response to load disturbance. What is going on?

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Lecture 3 – Outline

- Disturbance models
 - Stochastic processes
 - Filtering of white noise
 - Spectral factorization



Response to reference change:

$$G_{yr}(s) = \frac{PC}{1+PC} = \frac{1}{s+1}$$

Reference to load disturbance:

$$G_{yd}(s) = \frac{P}{1 + PC} = \frac{s}{s^2 - 1} = \frac{s}{(s+1)(s-1)}$$

The control system is not internally stable!

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Two main types of disturbances



Process (or load) disturbances d

- Disturbances that affect the controlled process variables z
 - d_m measurable, can use feedforward to cancel them
 - d_n unmeasurable, must use feedback. Controller should have high gain at the dominant frequencies to supress them

Measurement disturbances n

- Disturbances that corrupt the feedback signals
 - Controller should have low gain at the dominant frequencies to avoid being "fooled"





Mini-problem

Deterministic disturbance models , e.g., impulse, step, ramp, sinusoidal signals	What linear systems $G(s)$ can generate the following deterministic disturbances?
 Can be modeled by Dirac impulse filtered through linear system 	 A step
 Stochastic disturbance models Common model: Gaussian stochastic process Can be modeled by white noise filtered through linear system Reasonable model for many real-world random fluctuations 	 A ramp
	A sinusoidal



Stochastic process – definition

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A **stochastic process** is a family of random variables $\{x(t), t \in T\}$

Can be viewed as a function of two variables, $x = x(t, \omega)$:

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- Fixed $\omega = \omega_0$ gives a time function $x(\cdot, \omega_0)$ (realization)
- Fixed $t = t_1$ gives a random variable $x(t_1, \cdot)$ (distribution)



For a **Gaussian process**, $x(t_1, \cdot)$ has a normal distribution



Gaussian processes

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We will mainly work with zero-mean stationary Gaussian processes.

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Mean-value function:

$$m_x = \mathbf{E} \, x(t) \equiv 0$$

Covariance function:

$$r_x(\tau) = \mathbf{E} x(t+\tau) x(t)^T$$

Cross-covariance function:

$$r_{xy}(\tau) = \mathbf{E} \, x(t+\tau) y(t)^T$$

A zero-mean stationary Gaussian process is completely characterized by its covariance function.



function:

By inverse Fourier transform

The **spectral density** or **spectrum** of a stationary stochastic

 $\Phi_x(\omega) := \int^\infty r_x(t) e^{-i\omega t} dt$

 $r_x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{i\omega t} \Phi_x(\omega) \, d\omega$

 $\operatorname{E} x(t)x^{T}(t) = r_{x}(0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \Phi_{x}(\omega) \, d\omega$

White noise

In particular, the **stationary (co)variance** is given by

Describes the distribution of power over different frequencies

process is defined as the Fourier transform of the covariance



Covariance fcn, spectral density, and realization



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White noise with intensity R_w is a random process w with constant spectrum

$$\Phi_w(\omega) = R_w$$

- Variance is infinite not physically realizable
- Can be interpreted as a train of random Dirac impulses
- When filtered through a stable LTI system, the output is a zero-mean stationary Gaussian process

Filtering of white noise



Assume w white noise with intensity R_w . Two modeling/analysis problems:

- Given G(s) (or (A, B, C, D)), calculate the spectral density or stationary variance of y (or x)
- Onversely, given the spectral density of y, determine a stable G(s) that generates that spectrum
 - Known as spectral factorization



Calculation of spectrum – transfer function form



Calculation of spectrum – state-space form



Given stable G(s) and input w with the spectral density $\Phi_w(\omega)$. Then output y gets the spectrum

$$\Phi_{v}(\omega) = G(i\omega)\Phi_{w}(\omega)G^{*}(i\omega)$$

Special case: If
$$w$$
 is white noise with intensity R_w , then

$$\Phi_{\rm v}(\omega) = G(i\omega)R_{\rm w}G^*(i\omega)$$



Assume a stable linear system with white noise input

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 $\dot{x} = Ax + Bw, \qquad \Phi_w(\omega) = R_w$

The transfer function from w to x is

$$G(s) = (sI - A)^{-1}B$$

and the spectrum for x will be

$$\Phi_x(\omega) = (i\omega I - A)^{-1} B R_w \underbrace{B^* (-i\omega I - A)^{-T}}_{G^*(i\omega)}$$

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Calculation of covariance – example

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Theorem 3.1

Given a stable linear system with white noise input

$$\dot{x} = Ax + Bw, \qquad \Phi_w(\omega) = R_w$$

then the stationary covariance of x is given by

$$\mathbf{E} x x^T = \frac{1}{2\pi} \int_{-\infty}^{\infty} \Phi_x(\omega) d\omega := \Pi_x$$

where $\Pi_x = \Pi_x^T > 0$ is given by the solution to the Lyapunov equation

$$A\Pi_x + \Pi_x A^T + BR_w B^T = 0$$

Consider the system

$$\dot{x} = Ax + Bw = \begin{bmatrix} -1 & 2 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} w$$

where w is white noise with intensity 1.

What is the stationary covariance of *x*?

First check the eigenvalues of $A: \lambda = -\frac{1}{2} \pm i\frac{\sqrt{7}}{2} \in LHP$. OK!

Solve the Lyapunov equation $A\Pi_x + \Pi_x A^T + BR_w B^T = 0_{2,2}$.





Theorem 3.2

Spectral factorization

Assume that the scalar spectral density function $\Phi_w(\omega) \ge 0$ is a rational function of ω^2 and finite for all ω . Then there exists a rational function G(s) with all poles in the left half-plane and all zeros in the left half-plane or on the imaginary axis such that

 $\Phi_{w}(\omega) = |G(i\omega)|^{2} = G(i\omega)G(-i\omega)$

 $A\Pi_x + \Pi_x A^T + BR_w B^T = 0_{2\times 2}$

Find Π_x :

$$\begin{bmatrix} -1 & 2 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} \Pi_{11} & \Pi_{12} \\ \Pi_{12} & \Pi_{22} \end{bmatrix} + \begin{bmatrix} \Pi_{11} & \Pi_{12} \\ \Pi_{12} & \Pi_{22} \end{bmatrix} \begin{bmatrix} -1 & -1 \\ 2 & 0 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \end{bmatrix} =$$
$$= \begin{bmatrix} 2(-\Pi_{11} + 2\Pi_{12}) + 1 & -\Pi_{12} + 2\Pi_{22} - \Pi_{11} \\ -\Pi_{12} + 2\Pi_{22} - \Pi_{11} & -2\Pi_{12} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$

Solving for $\Pi_{11},\,\Pi_{12}$ and Π_{22} gives

$$\Pi_x = \begin{bmatrix} \Pi_{11} & \Pi_{12} \\ \Pi_{12} & \Pi_{22} \end{bmatrix} = \begin{bmatrix} 1/2 & 0 \\ 0 & 1/4 \end{bmatrix} > 0$$

Matlab: lyap([-1 2; -1 0], [1; 0]*[1 0])

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Spectral factorization — example

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Lecture 3 – summary

Find a stable, minimum-phase filter G(s) such that a process y generated by filtering unit intensity white noise through G gives

$$\Phi_{y}(\omega) = \frac{\omega^2 + 4}{\omega^4 + 10\omega^2 + 9},$$

Solution. We have

$$\Phi_{y}(\omega) = \frac{\omega^{2} + 4}{(\omega^{2} + 1)(\omega^{2} + 9)} = \left|\frac{i\omega + 2}{(i\omega + 1)(i\omega + 3)}\right|^{2}$$

implying

$$G(s) = \frac{s+2}{(s+1)(s+3)}$$

- Look at all important closed-loop transfer functions: Gang of four / gang of six
- White noise filtered through LTI system gives Gaussian stochastic process – simple but useful disturbance model
- Calculation of spectrum and stationary covariance given generating system
- Calculation of generating system given spectrum (spectral factorization)