





A **system** is a mapping from the input signal u(t) to the output signal y(t), $-\infty < t < \infty$:

Automatic Control LTH, 2018

 $y = \mathcal{S}(u)$



System properties



System properties (cont'd)

Lecture 1 FRTN10 Multivariable Control

A system ${\cal S}$ is

Signals and systems

System representations

• Signal norm and system gain

- **causal** if $y(t_1)$ only depends on u(t), $-\infty < t \le t_1$, **non-causal** otherwise
- static if y(t₁) only depends on u(t₁),
 dynamic otherwise
- discrete-time if u(t) and y(t) are only defined for a countable set of discrete time instances t = tk, k = 0, ±1, ±2, ..., continuous-time otherwise

A system ${\mathcal S}$ is

- **single-variable** or **scalar** if *u*(*t*) and *y*(*t*) are scalar signals, **multivariable** otherwise
- time-invariant if y(t) = S(u(t)) implies $y(t + \tau) = S(u(t + \tau))$, time-varying otherwise
- linear if $S(\alpha_1 u_1 + \alpha_2 u_2) = \alpha_1 S(u_1) + \alpha_2 S(u_2)$, nonlinear otherwise



LTI system representations



State-space models

х

We will mainly deal with continuous-time **linear time-invariant** (LTI) systems in this course

For LTI systems, the same input–output mapping \mathcal{S} can be represented in a number of equivalent ways:

- linear ordinary differential equation
- linear state-space model
- transfer function
- impulse response
- step response
- frequency response
- . . .

Automatic Control LTH, 2018 Lecture 1 FRTN10 Multivariable Control



Mini-problem 1



Mini-problem 1

Lecture 1 FRTN10 Multivariable Control



How many states, inputs and outputs?

Determine the matrices A, B, C, D to write the system as

Automatic Control LTH, 2018

$$\begin{cases} \dot{x} = Ax + Bu\\ y = Cx + Du \end{cases}$$

Linear state-space model:

$$\begin{cases} \dot{x} = Ax + Bu\\ y = Cx + Du \end{cases}$$

Solution:

$$y(t) = Ce^{At}x(0) + \int_0^t Ce^{A(t-\tau)}Bu(\tau)d\tau + Du(t)$$

Automatic Control LTH, 2018



Impulse response

$$\begin{cases} \dot{x} = Ax + Bu\\ y = Cx + Du \end{cases}$$

Change of coordinates

$$z = Tx$$
, T invertible

$$\begin{cases} \dot{z} = T\dot{x} = T(Ax + Bu) = T(AT^{-1}z + Bu) = TAT^{-1}z + TBu \\ y = Cx + Du = CT^{-1}z + Du \end{cases}$$



Automatic Control LTH, 2018 Lecture 1 FRTN10 Multivariable Control



Step response



Common experiment in process industry





Common experiment in medicine and biology



Transfer function



 $G(s) = \mathcal{L}\{g(t)\}$

$$y(t) = (g * u)(t) \quad \Leftrightarrow \quad Y(s) = G(s)U(s)$$

Conversion from state-space form to transfer function:

$$G(s) = C(sI - A)^{-1}B + D$$



A transfer function is **rational** if it can be written as

$$G(s) = \frac{B(s)}{A(s)}$$

where B(s) and A(s) are polynomials in s

- Example of non-rational function: Time delay e^{-sL}
- It is **proper** if deg $B \le \deg A$ and **strictly proper** if deg $B < \deg A$
 - Example of non-proper function: Pure derivative *s*
- A rational and proper transfer function can be converted to state-space form (see Collection of Formulae)



Automatic Control LTH, 2018 Lecture 1 FRTN10 Multivariable Control



The Nyquist diagram





Frequency response



Assume stable transfer function G = Lg. Input $u(t) = \sin \omega t$ gives

$$y(t) = \int_0^t g(\tau)u(t-\tau)d\tau = \operatorname{Im}\left[\int_0^t g(\tau)e^{-i\omega\tau}d\tau \cdot e^{i\omega\tau}\right]$$
$$\to \infty] = \operatorname{Im}\left(G(i\omega)e^{i\omega\tau}\right) = |G(i\omega)|\sin\left(\omega t + \arg G(i\omega)\right)$$

After a transient, also the output becomes sinusoidal

Automatic Control LTH, 2018 Lecture 1 FRTN10 Multivariable Control



[*t* ·

The Bode diagram



Each new factor enters additively!



01 OL

10

10

The Bode diagram

10

10



Signal norm and system gain



How to quantify

• the "size" of the signals *u* and *y*

• the "maximum amplification" between *u* and *y*



10⁰

Signal norm



Automatic Control LTH, 2018 Lecture 1 FRTN10 Multivariable Control

System gain

The L_2 norm of a signal $y(t) \in \mathbb{R}^n$ is defined as

$$\|y\| = \sqrt{\int_0^\infty |y(t)|^2 dt}$$

By Parseval's theorem it can also be expressed as

$$\|y\| = \sqrt{\frac{1}{2\pi} \int_{-\infty}^{\infty} |Y(i\omega)|^2 d\omega}$$

The L_2 (or " L_2 -induced") gain of a general system S with input u and output S(u) is defined as

$$\|\mathcal{S}\| := \sup_{u} \frac{\|\mathcal{S}(u)\|}{\|u\|}$$





Mini-problem 2

Theorem 1.1

Consider a stable LTI system S with transfer function G(s). Then

$$\|\mathcal{S}\| = \sup_{\omega} |G(i\omega)| := \|G\|_{\infty}$$

Proof. Let $y = \mathcal{S}(u)$. Then

$$||y||^{2} = \frac{1}{2\pi} \int_{-\infty}^{\infty} |Y(i\omega)|^{2} d\omega = \frac{1}{2\pi} \int_{-\infty}^{\infty} |G(i\omega)|^{2} |U(i\omega)|^{2} d\omega \le ||G||_{\infty}^{2} ||u||^{2}$$

The inequality is arbitrarily tight when u(t) is a sinusoid near the maximizing frequency.

(How to interpret $|G(i\omega)|$ for matrix transfer functions will be explained in Lecture 2.)



Automatic Control LTH, 2018 Lecture 1 FRTN10 Multivariable Control





What are the L_2 gains of the following scalar LTI systems?





Lecture 1 FRTN10 Multivariable Control

- Course overview
- Review of LTI system descriptions (see also Exercise 1)
- L_2 norm of signals

• Definition:
$$||y|| := \sqrt{\int_0^\infty |y(t)|^2 dt}$$

Automatic Control LTH. 2018

• L_2 gain of systems

• Definition:
$$||S|| := \sup_{u} \frac{||S(u)||}{||u||}$$

• Special case—stable LTI systems: $||S|| = \sup_{\omega} |G(i\omega)| := ||G||_{\infty}$ (also known as the " H_{∞} norm" of the system)