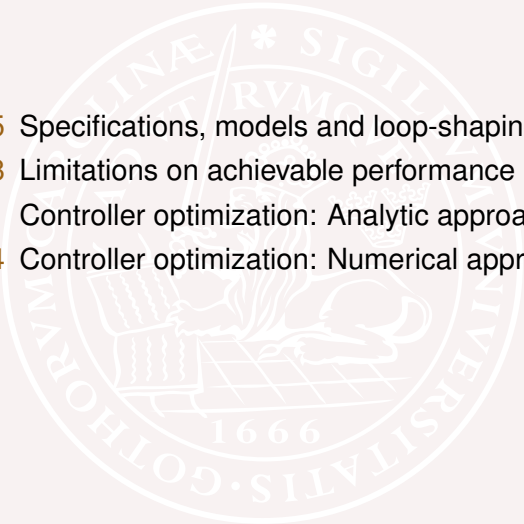


Course outline

- 
- L1-L5 Specifications, models and loop-shaping by hand
 - L6-L8 Limitations on achievable performance
 - L9-L11 Controller optimization: Analytic approach
 - L12-L14 Controller optimization: Numerical approach

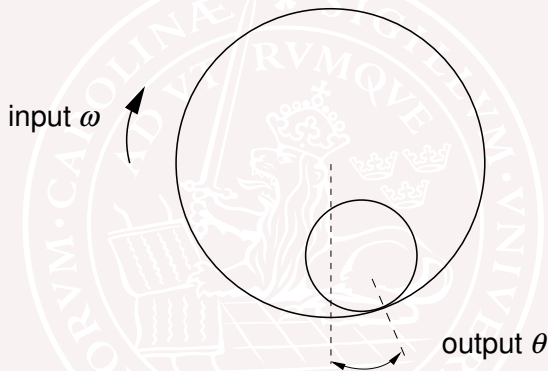
Lecture 6

- Controllability and observability
- Multivariable zeros
- Realizations on diagonal form

Examples: Ball in a hoop
Multiple tanks

[Glad & Ljung] Ch. 3.2–3.3, notes on course web page

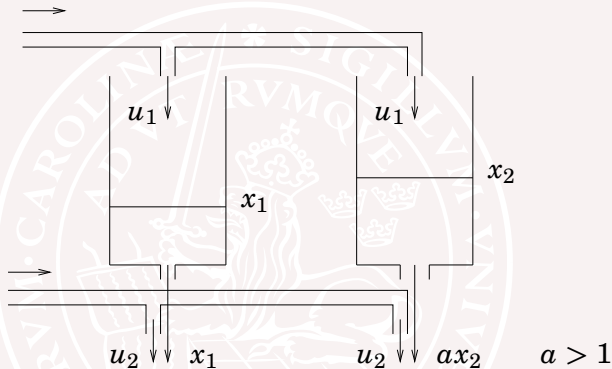
Example: Ball in the Hoop



$$\ddot{\theta} + c\dot{\theta} + k\theta = \dot{\omega}$$

Can you reach $\theta = \pi/4$, $\dot{\theta} = 0$? Can you stay there?

Example: Two water tanks



$$\begin{aligned}\dot{x}_1 &= -x_1 + u_1 & y_1 &= x_1 + u_2 \\ \dot{x}_2 &= -ax_2 + u_1 & y_2 &= ax_2 + u_2\end{aligned}$$

Can you reach $y_1 = 1, y_2 = 2$?

Can you stay there?

Controllability

The system

$$\dot{x}(t) = Ax(t) + Bu(t)$$

is controllable , if for every $x_1 \in \mathbf{R}^n$ there exists $u(t), t \in [0, t_1]$, such that $x(t_1) = x_1$ is reached from $x(0) = 0$.

The collection of vectors x_1 that can be reached in this way is called the controllable subspace.

Controllability criteria

The following statements regarding a system $\dot{x}(t) = Ax(t) + Bu(t)$ of order n are equivalent:

- (i) The system is controllable
- (ii) $\text{rank} [A - \lambda I \quad B] = n$ for all $\lambda \in \mathbf{C}$
- (iii) $\text{rank} [B \quad AB \quad \dots \quad A^{n-1}B] = n$

If A is exponentially stable, define the controllability Gramian

$$S = \int_0^\infty e^{At} B B^T e^{A^T t} dt$$

For such systems there is a fourth equivalent statement:

- (iv) The controllability Gramian is non-singular

Interpretation of the controllability Gramian

The controllability Gramian measures how difficult it is in a stable system to reach a certain state.

In fact, let $S_1 = \int_0^{t_1} e^{At} B B^T e^{A^T t} dt$. Then, for the system $\dot{x}(t) = Ax(t) + Bu(t)$ to reach $x(t_1) = x_1$ from $x(0) = 0$ it is necessary that

$$\int_0^{t_1} |u(t)|^2 dt \geq x_1^T S_1^{-1} x_1$$

Equality is attained with

$$u(t) = B^T e^{A^T(t_1-t)} S_1^{-1} x_1$$

Proof

$$\begin{aligned} 0 &\leq \int_0^{t_1} [x_1^T S_1^{-1} e^{A(t_1-t)} B - u(t)^T] [B^T e^{A^T(t_1-t)} S_1^{-1} x_1 - u(t)] dt \\ &= x_1^T S_1^{-1} \int_0^{t_1} e^{At} B B^T e^{A^T t} dt S_1^{-1} x_1 \\ &\quad - 2x_1^T S_1^{-1} \int_0^{t_1} e^{A(t_1-t)} B u(t) dt + \int_0^{t_1} |u(t)|^2 dt \\ &= -x_1^T S_1^{-1} x_1 + \int_0^{t_1} |u(t)|^2 dt \end{aligned}$$

so $\int_0^{t_1} |u(t)|^2 dt \geq x_1^T S_1^{-1} x_1$ with equality attained for $u(t) = B^T e^{A^T(t_1-t)} S_1^{-1} x_1$. This completes the proof.

Computing the controllability Gramian

The controllability Gramian $S = \int_0^\infty e^{At} B B^T e^{A^T t} dt$ can be computed by solving the linear system of equations

$$AS + SA^T + BB^T = 0$$

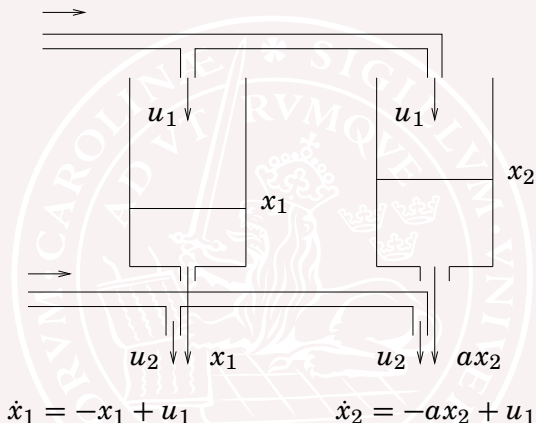
Proof. A change of variables gives

$$\int_h^\infty e^{At} B B^T e^{A^T t} dt = \int_0^\infty e^{A(t-h)} B B^T e^{A^T (t-h)} dt$$

Differentiating both sides with respect to h and inserting $h = 0$ gives

$$-BB^T = AS + SA^T$$

Example: Two water tanks



The controllability Gramian $S = \int_0^\infty \begin{bmatrix} e^{-t} \\ e^{-at} \end{bmatrix} \begin{bmatrix} e^{-t} \\ e^{-at} \end{bmatrix}^T dt = \begin{bmatrix} \frac{1}{2} & \frac{1}{a+1} \\ \frac{1}{a+1} & \frac{1}{2a} \end{bmatrix}$

is close to singular when $a \approx 1$. Interpretation?

Example cont'd

In matlab you can solve the Lyapunov equation $AS + SA^T + BB^T = 0$ by `lyap`

```
>> a=1.25 ;   A=[-1 0 ; 0 -1*a] ; B=[1 ; 1] ;
```

```
>> Cs= [B  A*B] , rank(Cs)
```

```
Cs =
```

```
    1.0000    -1.0000
```

```
    1.0000    -1.2500
```

```
ans =
```

```
    2
```

```
>> S=lyap(A,B*B')
```

```
S =
```

```
    0.5000    0.4444
```

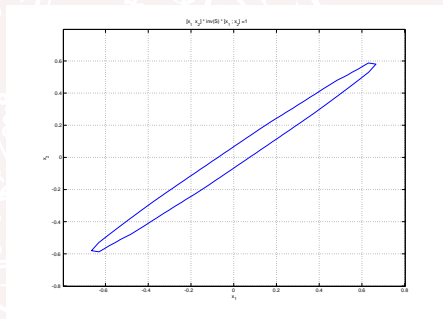
```
    0.4444    0.4000
```

```
>> invS=inv(S)
```

```
invS =
```

```
   162.0  -180.0
```

```
  -180.0   202.5
```



Plot of $\begin{bmatrix} x_1 & x_2 \end{bmatrix} \cdot S^{-1} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = 1$

corresponds to the states we can reach by

$$\int_0^\infty |u(t)|^2 dt = 1.$$

Observability

The system

$$\dot{x}(t) = Ax(t)$$

$$y(t) = Cx(t)$$

is observable , if the initial state $x(0) = x_0 \in \mathbf{R}^n$ is uniquely determined by the output $y(t), t \in [0, t_1]$.

The collection of vectors x_0 that cannot be distinguished from $x = 0$ is called the unobservable subspace.

Observability criteria

The following statements regarding a system $\dot{x}(t) = Ax(t)$, $y(t) = Cx(t)$ of order n are equivalent:

- (i) The system is observable
- (ii) $\text{rank} \begin{bmatrix} A - \lambda I \\ C \end{bmatrix} = n$ for all $\lambda \in \mathbb{C}$
- (iii) $\text{rank} \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix} = n$

If A is exponentially stable, define the observability Gramian

$$O = \int_0^{\infty} e^{A^T t} C^T C e^{A t} dt$$

For such systems there is a fourth equivalent statement:

- (iv) The observability Gramian is non-singular

Interpretation of the observability Gramian

The observability Gramian measures how difficult it is in a stable system to distinguish two initial states from each other by observing the output.

In fact, let $O_1 = \int_0^{t_1} e^{A^T t} C^T C e^{A t} dt$. Then, for $\dot{x}(t) = Ax(t)$, the influence from the initial state $x(0) = x_0$ on the output $y(t) = Cx(t)$ satisfies

$$\int_0^{t_1} |y(t)|^2 dt = x_0^T O_1 x_0$$

Computing the observability Gramian

The observability Gramian $O = \int_0^\infty e^{A^T t} C^T C e^{A t} dt$ can be computed by solving the linear system of equations

$$A^T O + O A + C^T C = 0$$

Proof. The result follows directly from the corresponding formula for the controllability Gramian.

Poles and zeros

$$Y(s) = \underbrace{[C(sI - A)^{-1}B + D]}_{G(s)} U(s)$$

For scalar systems, the points $p \in \mathbb{C}$ where $G(s) = \infty$ are called poles of G . They are eigenvalues of A and determine stability. The poles of $G(s)^{-1}$ are called zeros of G .

This definition can be used also for square systems, but we will next give a more general definition, involving also multiplicity.

Pole polynomial and Zero polynomial

- The pole polynomial is the least common denominator of all minors (sub-determinants) to $G(s)$.
- The zero polynomial is the greatest common divisor of the maximal minors of $G(s)$.

The poles of G are the roots of the pole polynomial.

The zeros of G are the roots of the zero polynomial.

When $G(s)$ is square, the only maximal minor is $\det G(s)$, so the zeros are determined from the equation

$$\det G(s) = 0$$

For a minimal and square realization, zeros are the solutions to

$$\det \begin{bmatrix} sI - A & B \\ -C & D \end{bmatrix} = 0$$

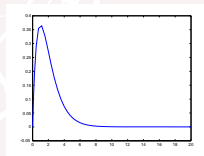
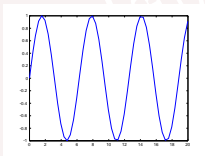
Interpretation of poles and zeros

Poles:

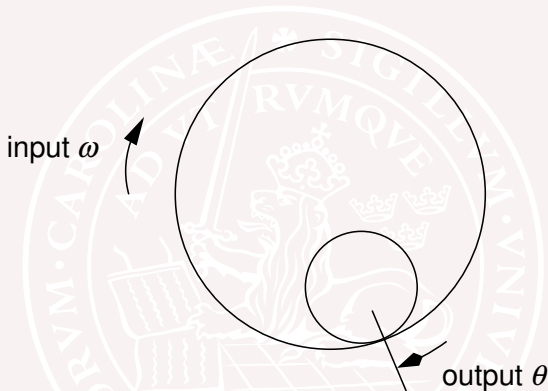
- A pole $s = \alpha$ is associated with a time function $x(t) = x_0 e^{\alpha t}$
- A pole $s = \alpha$ is an eigenvalue of A

Zeros:

- A zero $s = \alpha$ means that an input $u(t) = u_0 e^{\alpha t}$ is blocked
- A zero describes how inputs and outputs couple to states



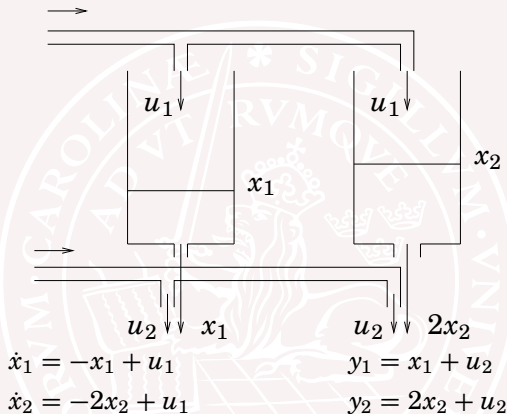
Example: Ball in the Hoop



$$\ddot{\theta} + c\dot{\theta} + k\theta = \dot{\omega}$$

The transfer function from ω to θ is $\frac{s}{s^2 + cs + k}$. The zero in $s = 0$ makes it impossible to control the stationary position of the ball.

Example: Two water tanks



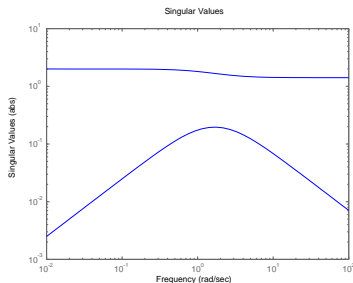
$$G(s) = \begin{bmatrix} \frac{1}{s+1} & 1 \\ \frac{2}{s+2} & 1 \end{bmatrix} \quad \det G(s) = \frac{-s}{(s+1)(s+2)}$$

The system has a zero in the origin! At stationarity $y_1 = y_2$.

Plot Singular Values of $G(s)$ Versus Frequency

```
» s=tf('s')
» G=[1/(s+1) 1 ; 2/(s+2) 1]
» sigma(G) ; plot singular values

% ALT. for a certain frequency:
» i=sqrt(-1)
» w=1;
» A=[1/(i*w+1) 1 ; 2/(i*w+2) 1]
» [U,S,V] = svd(A)
```



The largest singular value of $G(i\omega) = \begin{bmatrix} \frac{1}{i\omega+1} & 1 \\ \frac{2}{i\omega+2} & 1 \end{bmatrix}$ is fairly constant. This is due to the second input. The first input makes it possible to control the difference between the two tanks, but mainly near $\omega = 1$ where the dynamics make a difference.

Singular values - continued

Revisit example from lecture notes 2:

The largest singularvalue of a matrix A , $\bar{\sigma}(A) = \sigma_{max}(A)$ is the square root of the largest eigenvalue of the matrix A^*A ,

$$\bar{\sigma}(A) = \sqrt{\lambda_{max}(A^*A)}$$

Q: For frequency specifications (see prev lectures); When are we interested in the largest amplification and when are we interested in the smallest amplification?

Realization on diagonal form

Consider a transfer matrix with partial fraction expansion

$$G(s) = \sum_{i=1}^n \frac{C_i B_i}{s - p_i} + D$$

This has the realization

$$\dot{x}(t) = \begin{bmatrix} p_1 I & & 0 \\ & \ddots & \\ 0 & & p_n I \end{bmatrix} x(t) + \begin{bmatrix} B_1 \\ \vdots \\ B_n \end{bmatrix} u(t)$$

$$y(t) = [C_1 \quad \dots \quad C_n] x(t) + D u(t)$$

The rank of the matrix $C_i B_i$ determines the necessary number of columns in B_i and the multiplicity of the pole p_i .

Example: Realization of Multi-variable system

To find state space realization for the system

$$G(s) = \begin{bmatrix} \frac{1}{s+1} & \frac{2}{(s+1)(s+3)} \\ \frac{6}{(s+2)(s+4)} & \frac{1}{s+2} \end{bmatrix}$$

write the transfer matrix as

$$\begin{bmatrix} \frac{1}{s+1} & \frac{1}{s+1} - \frac{1}{s+3} \\ \frac{3}{s+2} - \frac{3}{s+4} & \frac{1}{s+2} \end{bmatrix} = \frac{\begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} 1 & 1 \end{bmatrix}}{s+1} + \frac{\begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} 3 & 1 \end{bmatrix}}{s+2} - \frac{\begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} 0 & 1 \end{bmatrix}}{s+3} - \frac{\begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} 3 & 0 \end{bmatrix}}{s+4}$$

This gives the realization

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \dot{x}_3(t) \\ \dot{x}_4(t) \end{bmatrix} = \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -2 & 0 & 0 \\ 0 & 0 & -3 & 0 \\ 0 & 0 & 0 & -4 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \\ x_4(t) \end{bmatrix} + \begin{bmatrix} 1 & 1 \\ 3 & 1 \\ 0 & -1 \\ -3 & 0 \end{bmatrix} \begin{bmatrix} u_1(t) \\ u_2(t) \end{bmatrix}$$
$$\begin{bmatrix} y_1(t) \\ y_2(t) \end{bmatrix} = \begin{bmatrix} 1 & 0 & 1 & 0 \\ 0 & 1 & 0 & 1 \end{bmatrix} x(t)$$

Summary

- Controllability and observability
- Multivariable zeros
- Realizations on diagonal form

Examples: Ball in a hoop
Multiple tanks

[Glad & Ljung] Ch. 3.2–3.3, notes on course web page